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Solar-Supplemented, Natural Air Drying of **Shelled Corn**

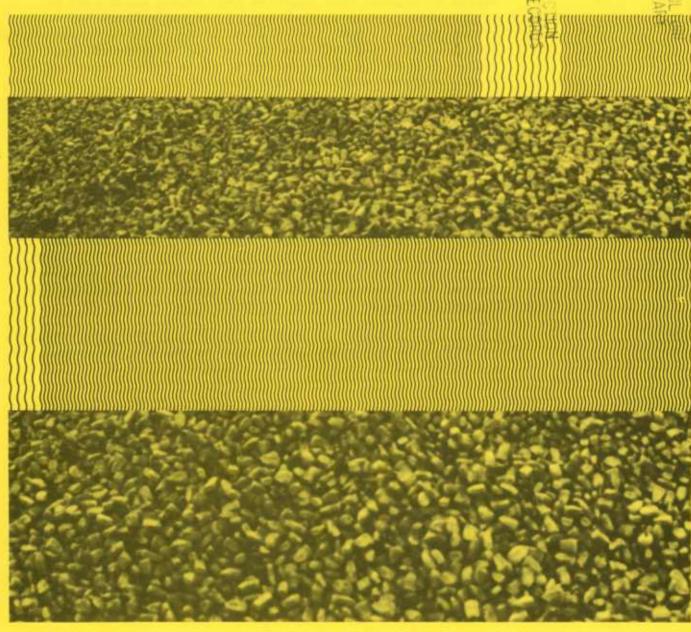
The Economic Limitations

Walter G. Heid, Jr. David F. Aldis









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ABSTRACT

It is not economically feasible to supplement natural air drying of high-moisture shelled corn by adding heat (solar and otherwise). In some cases, that drying method speeds product deterioration. A simulation analysis of the west central Great Plains determined that benefits from adding solar heat to batch-in-bin and layer-in-bin grain drying methods failed to offset the solar heat installation costs and product deterioration losses. Findings also suggest that high-speed, high-temperature drying is necessary to avoid field losses and to ensure marketable corn of high quality.

Keywords: Solar, Natural air, Grain drying, Cost, Corn quality, Simulation.

NOTES

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SIIMMARY

Adding solar heat or any other form of low-temperature supplemental heat to dry high-moisture shelled corn is not economically feasible compared with natural airflow drying. Solar-supplemented per-bushel costs far exceeded returns in the west central Great Plains, the corn-growing region with the highest average annual solar radiation.

The simulated analysis in this report used 20 years of weather and solar radiation data for Dodge City, Kans., an 8,000-bushel drying and storage system, and batch-in-bin and layer-in-bin drying methods. Price and cost data for the 1979/80 marketing year served as the economic base.

Supplemental solar heat had no effect on the batch-in-bin (single fill) strategy in good drying years, and failed to stem deterioration in poor drying years. High-moisture corn cannot be consistently preserved without using high-temperature dryers. Should fossil fuel for operating high-temperature grain dryers no longer be available, farmers insisting on fast harvest may choose to let their corn deteriorate a grade in poor drying years rather than invest in an uneconomical low-temperature dryer.

Layer-in-bin drying, although a method that could slow harvest, required no supplemental heat, even in years of high humidity after harvest. The addition of solar heat resulted in appreciable corn overdrying.

Results of a simulation model show that farmers can dry high-moisture corn more economically through natural airflow than by any form of supplemental heat, including solar energy. Farmers may allow more than 50 percent of their corn to deteriorate to grades No. 3 or 4 (low-quality corn), in poor drying years, and still lose less money than by installing a solar collector or some other supplemental heat source.

Solar-Supplemented, Natural Air Drying of Shelled Corn

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INTRODUCTION

Farmers can dry high-moisture corn more economically through natural airflow than if they use any form of low-temperature supplemental heat, including solar energy, according to results of this simulation model.

Solar grain drying, being a slow, low-temperature method, is more closely related to natural air drying. It cannot be used to rapidly dry large volumes of high-moisture grain. Recognizing the limited role of solar grain drying and the costs associated with backup units assumed in previous studies, this study analyzes the use of solar energy as a supplement to natural air drying.

Two popular methods of drying, batch-in-bin and layer-in-bin, were simulated, using variables of initial corn moisture content, date of harvest, and weather. Results are analyzed by days required for corn moisture content to reach a safe storage level, accumulated deterioration, and costs of drying relative to market discounts for low-quality corn.

The use of solar collectors as a means of low-temperature grain drying is widely described in engineering literature. Previous studies have cast solar collectors in a primary drying role, assuming the use of backup units in years of poor drying weather (12, 18).1/ Research results are frequently reported in terms of energy savings relative to high-speed, high-temperature conventional grain drying.

Solar-supplemented drying of shelled corn may be economically feasible when employing a multiple-use system to dry lower moisture corn (9).

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 $[\]underline{1}/$ Underlined numbers in parentheses cite references listed at the end of the report.

BACKGROUND AND VARIABLES

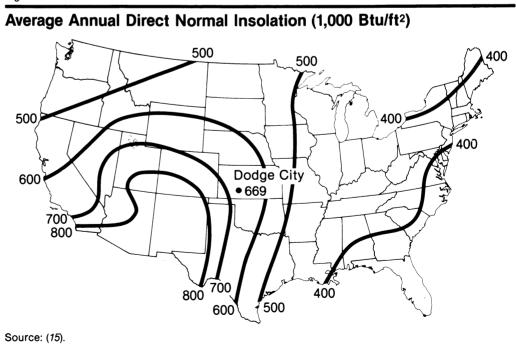
Several major factors such as delayed harvest, optional airflow needs (fan cost), the mixing of wet and dry corn, and the cash discounts for low-quality corn provide necessary input for computing costs and returns from grain drying and for making decisions on related strategies. Each of these factors affects situations in which a solar collector (supplemented heat) may enhance the drying of shelled corn, as well as situations when the use of a natural air system alone is most economical.

The west central Great Plains is generally considered to be an ideal location for harnessing solar energy. This region has the highest average annual insolation (incoming solar radiation) of any major corn-producing region. Climatological data for Dodge City, western Kansas, shows an average insolation of 669,000 British Thermal Units (Btu) per square foot annually (fig. 1). This compares with 400,000 to 500,000 Btu per square foot for most of the Corn Belt.

Weather Data

Twenty years (1955-74) of actual radiation and other weather data for Dodge City were used to predict performance of a natural air drying system with and without the input of a solar collection system. These data were obtained from solar and meteorological data tapes (SOLMET) purchased from the National

Figure 1



Climatic Center, Asheville, N.C. Twenty years of data gave more reliable results than only 10 years of data would have because of the exceptional number of excellent crop years in the late sixties and early seventies. (Often a good crop year is associated with higher than average moisture conditions, signifying poor drying conditions.) As the study progressed, choice of the longer series proved important as probabilities of failure in some simulation runs were twice as high for one 10-year period as for the other.

Even though the region selected for this study is one of high insolation and is generally considered to be a low-humidity area, the 20 years of weather data revealed periods of extremely high humidity during the September-October harvest months. Average relative humidity for the September-simulated runs ranged from 30 to 71 percent. For the October runs, it ranged from 37 to 75 percent. In years of high average humidity, readings commonly ran over 85 percent for several consecutive days during the dry season. This, of course, suggests that drying conditions in the west central Great Plains may not be much different from parts of the Corn Belt in certain years.

Grain Deterioration and Weight Losses

High-moisture shelled corn deteriorates if it is not dried fast enough. However, it loses weight even if dried properly. Weight losses result in economic losses since producers are paid by the weight of their product. So producers must balance economic losses from deterioration with economic losses from lighter weight corn. Ideally, they need a corn drying system that achieves the optimum moisture content in the shortest time with the least deterioration.

Deterioration results from mold growth that causes both oxidation and the loss of dry matter. The dry-matter loss caused by mold growth can be estimated if the grain temperature, its moisture content, and the length of time the grain is maintained at the moisture content are known. If corn loses 0.5-percent dry matter by mold deterioration it will decline by at least one grade $(\underline{12}, \underline{18})$. The allowable storage time for highmoisture shelled corn is shown in table 1. For more information concerning the loss of dry matter by mold deterioration, see (14).

When handled, shelled corn can also lose 0.5 percent of dry matter in the form of chaff and dust (5, 16). Such loss reduces the weight of the corn and affects its grade only if the fine material is not separated from the corn.

A bushel of 24-percent moisture corn contains 14.94 pounds of water, while a bushel of 15.5-percent moisture corn contains only 8.68 pounds. At 15.5-percent moisture, a bushel of corn

Table 1Allowable	storage	time	for	high-moisture	shelled	corn
------------------	---------	------	-----	---------------	---------	------

Corn storage	:		Con	rn moi	stur	e cont	ent	(perce	nt)	
temperature (degrees F)	: _:	18	:	20	:	22	:	24	:	26
	:					D.				
	•					Days				
80	:	17		9		5		4		3
75	:	23		12		7		5		4
70	:	31		16		9		6		5
65	:	42		21		13		8		6
	:									
60	:	56		28		17		11		8
55	:	85		42		25		16		12
50	:	128		63		37		25		18
45	:	192		95		56		37		27
	:									
40	:	288		142		84		56		41
35	:	432		214		126		85		62
30	:	648		321		190		127		94
0 /1	:									

Source: (11).

(by volume) weighs 56 pounds. A bushel (by volume) of 24-percent moisture corn weighs 62.26 pounds ($\underline{11}$). In effect, when moisture is removed, the weight of a bushel decreases. Since the price paid to farmers may be discounted for high moisture and low test weight, excess moisture reduction can mean lower profits.

For corn to be graded U.S. No. 1, it must have a minimum test weight of 56 pounds and a maximum moisture content of 14 percent. Requirements for No. 2 corn are a minimum of 54 pounds test weight and a maximum of 15.5-percent moisture content. For No. 3 corn, the requirements are 52 pounds for test weight and 17.5 percent for moisture. In each case, other factors are also considered (18).

Economic discounts given at the country elevator are based on U.S. No. 2 corn. Commonly, corn is discounted 1 to 1.5 cents a bushel for each 0.5-percent moisture above the standard 15.5 percent.

Values are quoted at major terminal markets for Nos. 2, 3, and 4 corn. The level of discount may vary from year to year depending on supply and demand. The amount of discount assumed

in this study was based on the difference between No. 2 corn and lower grades on the Kansas City market in the fall of 1979:

Grade	Average price	Discount
	Dollars per bushel	Cents per bushel
No. 2	2.80	0
No. 3	2.70	10
No. 4	2.54	26

Discounts caused by high-moisture content can be averted by onfarm drying. If, however, the drying system fails to dry corn properly every year, costs associated with the occasional losses in quality (grain deterioration) must be prorated over all years. If 8,000 bushels of corn were graded No. 3 instead of No. 2, the loss would be \$800, that is, 8,000 bushels x 10 cents. If, for example, a solar-supplemented, natural air drying system results in excessive dry-matter decomposition once every 10 years causing corn to be graded No. 3 instead of No. 2, the average annual loss would be 1 cent per bushel (table 2). If the system failed half of the time, the prorated cost would be 5 cents a bushel. On this basis, the probability of system failure is used to justify or reject the use of supplemental solar heat.

Table 2--Average annual economic loss due to corn quality deterioration

Grade reduction	:	Loss		ccurri mber o	_	_				ed
	:	1	:	2	:	3	:	4	:	5
	:			Ceı	nts	per b	ushe	<u>1</u>		
No. 2 to No. 3	:	0.010		0.020		0.030		0.040		0.050
No. 3 to No. 4	:	.016		.032		.048		.064		.080
No. 2 to No. 4	: :	.026		.052		.078		.104		.130

Delayed Harvest

Harvests that begin any time from early September through October usually involve high-moisture corn and coincide with warmer, more humid drying weather than harvests that begin in November or later. Although the FALDRY model used in this study indicated that corn harvested September 15 could be dried from 25-percent moisture to 15.5-percent moisture in fewer days than corn harvested on October 15, deterioration was much greater in the earlier period.

Delayed harvest increases the feasibility of using natural air drying or low-temperature drying, first, because the corn generally contains less moisture and, second, because ambient air temperatures are cooler and humidity is lower.

Farmers may intentionally delay harvest by leaving corn in the field until after the time when harvest, technically, could commence, or by planting later maturing varieties. Normally, leaving harvest-ready corn in the field could result in severe economic losses.

Expected loss emanates from kernel moisture, cob moisture, and time. Field losses start mounting as soon as kernel moisture drops below 25 to 26 percent. If farmers wait until their corn dries to 20-percent moisture before harvesting, much of it will shatter and be left in the field (2). In contrast, corn kernels are too soft and fragile above 26- to 28-percent moisture content to harvest mechanically. Harvesting losses steadily increase as corn is allowed to mature to lower moisture levels as follows:

Percent moisture	Percent loss
26	8.0
22	12.0
20	13.5
18	17.0
16	20.0

Field losses decrease to about 7.5 percent by harvesting at 28-percent moisture. At this point, the solid-matter content of corn is the highest. Once corn has matured to 26-percent moisture, the ear ceases to draw nourishment from the stalk, but moisture content is still high enough for respiration to continue. The respiration, or breathing, process consumes solids, thus increasing dry-matter losses.

Corn dries (loses moisture) at about three-fourths of a percent per day from the time it dents until it reaches about 25-percent moisture ($\underline{1}$). Corn at 25-percent moisture is normally unaffected by weather. However, after the moisture content drops below 25 percent, weather becomes a major factor. If

weather is favorable, corn in the 20- to 25-percent moisture range dries at an average daily rate of 0.5 percent. If the humidity is high, drying can take a month or more to reach 15.5-percent moisture. When corn is picked after remaining in the field over the same period, about 20 percent of the yield may be lost by conventional field shellers. Of this loss, one-third is in the form of ears and two-thirds is shelled kernels. Generally, for every two kernels of corn per square foot found in the field after harvest, a 1-bushel per acre field loss may be assumed.

For corn yielding 100 bushels per acre and valued at \$2.50 per bushel, a 20-percent loss equals \$50 per acre or 50 cents per bushel. At this rate, savings in field losses would more than cover the cost of drying.

Mixing Wet and Dry Corn

A study by Sauer and Burroughs (13) concluded that mixing wet and dry corn is a reasonably efficient way to save on drying costs, and a practice that may supplement limited drying system capacity. The practice of mixing wet and dry grain also may serve as an adjunct to low-energy, natural air drying systems. Equilibration of the wet and dry corn is rapid, usually more than 80-percent complete within 24 hours. 2/ Within 48 hours, equilibration averages 94-percent complete.

Blending does not cause quality loss in corn, provided the average moisture content of the blend is low enough to prevent fungal growth. However, some caution must be taken by both seller and buyer when blended corn is immediately marketed. If the wet corn is not thoroughly mixed with the dry corn, it is possible to get a wide range of moisture and test weight readings. However, if the corn is taken from the drying bin and placed in a storage bin, the amount of stirring may not be as critical. With continued aeration, no quality problems should be anticipated.

Another advantage of mixing wet and dry corn is the speed with which a farmer can reduce high moisture levels. The average moisture content reaches 15.5 percent about 1 week sooner than the top layer reaches this moisture level. (This assumes that 25-percent moisture corn is placed in the bin on October 15 in Dodge City.) If the corn can be moved from the drying bin when the average moisture reaches 15.5 percent, and the wet and dry kernels are mixed in the process, chances for mold growth may be greatly reduced.

^{2/} The term, equilibration, refers to the physiological process (in this case corn's) whereby all corn, wet and dry, reaches the same percentage of moisture by the transfer of moisture from wet kernels to dry kernels.

Fan and Heat Strategies

Three strategies were considered for drying:

- A 5-hp axial fan for moving heat from the solar collector into the corn bin and for longer term aeration. (A 5-hp fan is generally considered the largest practical fan size for aerating grain.)
- 2. A 10-hp axial fan for moving heat from the solar collector into the corn bin. (This fan size would be more expensive to operate, but it could produce a higher airflow and increase the probability of successful drying. For aeration, a fan of this size would normally be operated only a few minutes each day.)
- 3. A companion heater with option No. 1. Such heaters are capable of producing 2 million or more Btu's per hour and an airflow of 12,000 cubic feet per minute (cfm) at a temperature of 140° F.

Decisions to choose either of the first two options should be based on a comparison of the cost of owning and operating the solar collection system and the alternative (conventional) drying method. The value of anticipated losses in years of poor solar drying weather, as well as direct costs, must be taken into account.

The decision to choose a 10-hp fan over a 5-hp fan also must take into account the value of improved quality corn due to the larger fan as well as the added investment cost. At 1980 prices, the added cost of the larger fan amounted to 12 cents a bushel per year for the grain drying system selected for this study. If drying only one binful of corn, the added cost of the larger fan would likely exceed returns on better quality corn, even if the larger fan is needed every year.

If the third strategy is chosen, the decision should be based on the added cost of the heater versus savings in corn quality. The cost of owning and operating a supplemental heater must be compared with the loss due to corn deterioration. Since the heater would be used only sparingly, a 20-year lifespan may be assumed. The annual fixed cost of owning a backup heater would equal about 4.5 cents per bushel. Operating costs, assuming the use of an electric heater, would amount to nearly 13.5 cents per bushel. The economic loss due to corn deterioration, assuming a reduction in grade from No. 2 to No. 3 in 5 of 10 years, would be only 5 cents (table 2). Thus, it would not pay the farmer to maintain a backup unit for the system modeled in this study, given current fuel costs and discount schedules.

Instead, it would occasionally benefit farmers to sell lower grade corn. Therefore, as fuel costs and grain dryer investment costs (including solar collector costs) increase relative to corn prices, buyers should anticipate more and more poorquality corn, unless discounts for low-quality corn are raised. These conclusions may be applied to all crops presently dried in the west central Great Plains. In fact, in this region, where postharvest drying conditions are relatively favorable compared with other corn-producing areas, the use of any artificial drying method other than natural air is questionable. 3/

Capital Investment

Total investment for an 8,000-bushel system is estimated to be \$26,017, or \$3.38 per bushel (table 3). Components of the system and their percentages of total investment are:

Component	Percentage of total investment
Bins and accessories Handling equipment Aeration equipment Solar collector and equipment (2 months) Quality control	62.3 27.1 3.8 4.3 2.5
Total	100.0

Only one-sixth of the total cost of the solar collector and related equipment was included in this analysis. The remaining cost is assumed to be allocated to other farm use.

According to Linville (fig. 2), who studied in-bin systems ranging from 10,000 to 120,000 bushels (10), economies of scale exist in grain-drying and storage systems. The system designed for this study appears to be in line with the Linville investment curve. Thus, larger systems should reflect a considerably lower investment cost per bushel, particularly for bins and handling equipment. However, large-sized solar-supplemented, natural air drying systems may not achieve the maximum economies of scale shown in the Linville investment curve if the solar-supplemented system includes two or more small portable collectors attached in tandem.

SIMULATION MODEL

The FALDRY simulation model is used to predict the probability of economic loss due to quality deterioration of shelled corn

^{3/} Infield losses caused by corn borer infestation may be high enough in some cases to warrant harvesting and drying high-moisture corn.

Table 3--Capital investment costs of an 8,000-bushel grain-drying and storage system using solar energy to supplement natural air drying, 1980

Item	: :	Investment cost
	:	
D 1	:	<u>Dollars</u>
Bins and accessories:	:	
Bins <u>1</u> /	:	7,120
Floors, perforated $\underline{2}/$:	2,877
Foundations 3/	:	1,599
Spreaders <u>4</u> /	:	1,041
Labor	:	2,912
Miscellaneous (including fences and	:	
electric hookup)	:	655
Subtotal	:	16,204
	:	
Handling equipment:	:	
Elevating system $5/$:	3,631
Auger tube and screw 6/	:	2,088
Unloading motor	:	714
Grain cleaner	:	413
Labor	:	207
Subtotal	:	7,053
	:	•
Aeration equipment:	:	
Fan 7/	:	660
Transitions, ducts, and collars	:	330
Subtotal	:	990
	:	330
Solar collector and equipment:	:	
Collectors 8/ (2 months)	• •	639
Transitions, ducts, and collars	•	480
Subtotal	:	1,119
5 45 60 641	•	1,117
Quality control:	•	
(Humidistat, thermostat, manometer, and	•	
thermometer)	•	651
chermometer,	•	TCO
Total	•	26 017
10141	•	26,017

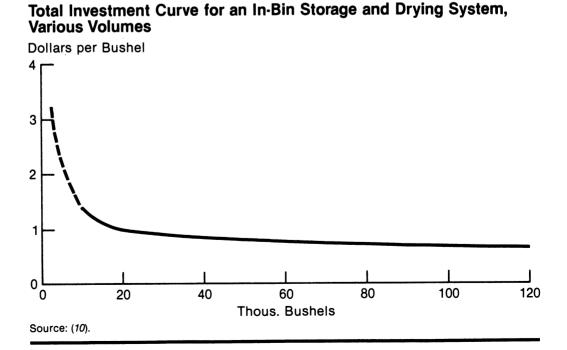
^{1/} Bin includes roof, 20 in. x 20 in. manway, anchor bolts, seam and base sealer, and base angle ring. 2/ Perforated floor, including plenum and metal supports. 3/ 18 in. of concrete. 4/ 0.25-hp motor. 5/ 6 in. electric auger designed at 30° angle for average sloped bin roofs; discharge directly into bin. 6/ 6 in. auger with 13 ft. vertical unloading auger electrically driven with motor mount connector sleeve and adjustable swivel spout. 7/ Electric heater and 5-hp 25 in. axial fan. Motor has prewind magnetic motor starter, overload relays, on-off breakers for each heat stage, interlock circuit between fan and heater, and is weather-protected. 8/ Flat-plate collectors.

(18). FALDRY is a deterministic model designed to simulate a system of one to six grain bins equipped with perforated floors and axial fans. Given bin specifications, fan sizes, grain pack factor, and harvest flow rates, the model: (1) allows total layer-filling flexibility by enabling each bin to accept any specified quantity of grain, (2) determines the air delivery rate and the resulting heat rise of the air based on fan and bin specifications and daily quantity of grain in the bin, (3) predicts the grain-moisture profile, drying time, and electricity usage, and (4) simulates a complete drying season. A series of simulation runs illustrate the effect of these factors and the addition of solar-supplemented heat on the drying process.

For batch-in-bin drying, initial runs showed that a 5-hp fan produced an airflow at 19.1 cfm per square foot of bin floor area. A 10-hp fan was required in years when drying was not accomplished without excess dry-matter decomposition, increasing the airflow to 24.3 cfm per square foot of bin floor area. These airflow rates represented 1.8 and 2.2 cfm per bushel, respectively.

For layer-in-bin drying, the initial airflow was 26.6 cfm per square foot of bin floor area. Airflow decreased as successive layers of shelled corn were added, eventually reaching the same

Figure 2



rate as the batch-in-bin system when the drying bin was ccm-pletely filled. A 10-hp fan was not modeled for layer-in-bin drying.

The FALDRY model predicts both the average amount of deterioration and the amount in each layer of the bin after each day of drying. System failure is predicted as the point where drymatter deterioration reaches 0.5 percent or more in the top layer. At this level of deterioration, corn quality of the entire bin is assumed to lose one grade point.

SYSTEM DESIGN

Batch methods, both in-bin and outside-bin systems, are the most common type of onfarm grain dryers. Outside-bin dryers use high temperatures and do not require bin space for the drying process. Batch-in-bin and layer-in-bin drying systems using lower temperatures are well adapted to a fast harvest so long as enough drying/storage space is available.

Batch-in-bin systems require more fan power than layer-in-bin systems because of greater grain depths. Therefore, a layer-in-bin system may be better suited to current and emerging farming practices that use conventional fuel by minimizing both the time and fuel requirements for drying. A recent grain dryer survey in Kansas showed that layer-in-bin systems have been the most frequent type of in-bin dryers purchased by farmers since 1976 (6).

A capacity of 8,000 bushels is assumed for the simulated drying/storage system. The bin configuration includes three 18-foot diameter bins, each 15 feet high. To achieve compatibility with low-temperature drying and to provide for a manageable collector size, three small bins are designed into the system instead of one large bin. Each bin has a capacity of about 2,700 bushels. Grain depth of each batch is about 13 feet. Given a 100-bushel per acre corn yield, a system of this size can handle about 80 acres of corn.4/ It is further assumed that the flat-plate solar collectors, being a part of a multiple use system, are available for 2 months each fall to dry high-moisture corn.

Bin size is kept constant for both drying methods. For layer-in-bin drying, results of the model are applicable whether the corn is stored in alternate bins each day or one bin is filled every other day.

^{4/} There should be no economic or technical barriers to enlarging this system through duplication. Substantial economies of scale may exist in larger grain storage systems. Preliminary research shows some economies of scale in solar collectors and related equipment (4).

Collector Sizing

Sizing of solar collectors was based on the following formula (11):

A portable flat-plate collector was assumed, as was adjustment of the collector's airflow, to make it usable for home heating or other uses.

To obtain a 3-degree (F) temperature rise above the ambient air temperature, 363 square feet of collector surface was needed, or a 10- by 36-foot collector. That is, the ratio of collector surface to bin floor area was nearly 1.5 to 1 for the Dodge City area, assuming a 55-percent average collector efficiency, an easily obtainable percentage for homemade collectors.

Airflow rate is the most important factor in designing and operating batch-drying systems. A minimum airflow requirement for 24- to 26-percent moisture corn is 2 cfm per bushel. In poor drying weather, higher airflow is necessary to prevent spoilage. According to Converse, a drying fan and motor should be selected to provide an airflow volume of 30 cfm per square foot of the cross-sectional bin area (3). A 5-hp axial fan will produce the cfm required for an 18-foot diameter bin, assuming as much as 3 inches of static pressure (SP).5/ A 5-hp

fan may produce up to 5,000 cfm with 4 inches SP.

For this study, a 5-hp axial fan was used both on the solar collector for drying and later on the bin for aeration. A 5-hp fan is considered optimum since it is the largest size normally used for aeration following drying and the smallest that can be used on the collector considering airflow requirements. A 10-hp fan was considered for use in inclement years as an alternative to a backup heater. Both fans were assumed to carry a thermostat and humidistat.

A drying system must be designed to reduce the moisture content of high-moisture corn in less than 1 week if temperatures are high (table 1). However, once the corn is dried to 20-percent moisture, and grain temperature is below 60°F, time is less critical. A solar-supplemented, natural air drying system

Air System

^{5/} Static pressure is a measure of air pressure usually expressed in inches of water column (w.c.). Fans are rated in terms of static pressure and total air volumetric airflow.

could take a total of 30 or more days without serious grain quality loss.

SIMULATION RESULTS

Farmers will not benefit economically from solar-supplemental heat, using either batch-in-bin or layer-in-bin drying. Increased deterioration, longer drying time, and overdrying during batch-in-bin simulations cut into profits. The layer-in-bin method showed improved results but was plagued by unacceptable overdrying.

Batch-in-bin Drying

Two solar drying strategies were simulated for batch-in-bin drying. One was a single-bin strategy that assumed the corn was dried and stored in the same bin. The other was a transfer strategy that assumed the corn was dried to a 15.5-percent average moisture content and then transferred to a storage bin. For each strategy, September 15 to October 15 were the simulated harvest dates. Corn moisture was allowed to vary from 25 to 22 percent, and both 5- and 10-hp fans were used. For each simulation run, three levels of temperature rises were assumed. The first level assumed only the heat generated from The second level assumed 3 degrees (F) additional the fan. solar heat, and the third, 6 degrees (F) additional heat supplied by a solar collector. Total temperature rises, including fan-generated heat were, 2.7, 5.7, and 8.7 degrees (F), respectively.

Probabilities of success were determined for each simulation run, a successful year being one in which corn was dried to 15.5-percent moisture content without deterioration of the top layer reaching 0.5 percent.

Single-bin Strategy

The single-bin strategy may be a more realistic choice than a tranfer strategy on small farms with few bins, for farms with widely dispersed bins, and in cases where corn is custom harvested. With larger volumes of corn being stored on farms until well after harvest, the opportunity decreases for filling each bin more than once. Also, the uncertainty of drying time associated with low-temperature solar drying suggests a single fill.

September 15 Harvest Date. The time required to dry the top layer of corn to 15.5-percent moisture averaged 23 days using the 5-hp fan only, and 19 days when 6 degrees (F) of solar heat were applied (table 4). The temperature rise led to a decrease in corn deterioration 70 percent of the time and an increase 30 percent of the time. Chance of success (at or below 0.5-percent loss) was only 1 in 20 at all levels of temperature rise.

A second simulation run was made, assuming the use of a 10-hp fan. Even with larger airflow and a slightly higher tempera-

Table 4--Days required to dry bin average and top layer to 15.5-percent moisture, and accumulated deterioration, assuming September 15 harvest date, 25-percent moisture corn, and 5-hp fan

	Temp	rise 2.	_	degrees (F)	Temp	. rise 5.	_	degrees (F)	Temp.	. rise 8.	7 degree	rees (F)
Year	A	Average	Top	layer	Av	Average	Top	layer	Av	erage	Top	layer
	Days	Deteri- s oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration
	No.	비	No.	Percent	No.	Percent	No.	Percent	No.	Percent	No.	Percent
1955	20	0.625	25	68	15	49	22	50	13	4	19	28
1956	·	.154	14	.37		.15	13	.39	7	.163	12	41
1957	: 15	.307	21	77		28	19	75	11	7	18	73
1958	: 16	.482	22	.940	14	.475	20	.933	12	. 448	19	. 989
1959	. 18	.470	25	01		77	21	98	11	4	8 T	y
1960		787	22	12	14	.411	20	90		37		1.006
1961	19	. 278	22	.574	15	. 2	21	.603	13	.268	19	.623
1962	: 23	606	30	.65	19	7	26	.17		.615		•
1963	: 15	.657	21	37	13	9	19	37		61		1.392
1964	: 19	.531	25	.94	17	.507	23	.98		.475		•
170		r,	30	ار ب	20	717		13		43	24	90
1907		177	ט ני	ά.	7 -	887		76			20	96.
1967	. TO	351	200	2,7	12	377		82		30	17	79
1067		2 6	γ α	, ₇	1	300		78		28	16	73
1968 1969	17	.805	10 24	2.183	16	.746	21	1.944	14	.672	20	1.845
	••										,	(
1970	: 18	7	25	1.286	16	.524	22	1.147	14	.512	20	1.202
1971	: 18	6	24	77		2	21	77		.184	T ?	7.3
1972	: 14	9	20	.83		2	18	.84		.341	16	. 85
1973	: 21	2	27	41		$\overline{}$	25	27		.450	7.7	23
1974	: 16	.386	23	90		∞	21	81		.374	19	81
Average	: 17	9/4.	23	1.132	15	.438	21	1.063	13	404.	19	1.016
æ												
of success (≥0.5%)		09		5		70		2		80		5

ture rise due to added heat from the larger fan, the probabilities of success did not increase. In poor drying years, the top layer deterioration still exceeded the 0.5-percent acceptable maximum.

These results indicated an aberration in the climatological data for the region. The comparison showed that, although temperature differences were not as pronounced, average daily humidity was considerably higher on the September 15 drying date than on October 15. Thus, in the west central Great Plains, low-temperature solar batch drying of 25-percent moisture corn could not be accomplished starting September 15.

Seeking the moisture content at which solar-supplemental heat might make the difference between success and failure for the single-bin strategy, a third set of simulations was run assuming 23-percent moisture. Results indicated that corn must be below 23-percent moisture for successful low-temperature solar batch drying, if harvested on September 15. The probability of success was increased to 60 percent with temperature increases of 2.7 degrees and 5.7 degrees (F) and to 70 percent with an 8.7-degree (F) temperature rise (table 5). However, adding solar-supplemental heat to natural air not only failed to prevent deterioration, but actually increased it in the top layer 35 percent of the time.

In a fourth simulation run, the effects of harvest moisture level were analyzed. For a selected poor drying year, ability to solar dry 22- and 25-percent moisture corn was compared, assuming the 5-hp fan (table 6). Results indicated a high degree of success when drying 22-percent moisture corn, because drying time was reduced and supplemental heat was unnecessary. The run also predicted a sharp increase in grain deterioration in years of inclement postharvest weather, leading to potential serious economic losses due to mold growth.

The feasibility of harvesting corn in September was not pursued because, in a practical sense, low-moisture corn cannot always be harvested then in the region studied. Most production in the area is on irrigated land, and only about 50 percent of the corn is mature (down to 25- to 26-percent moisture) by September 15.

October 15 Harvest Date. Simulated solar drying averaged 4 to 10 days longer than for the September 15 harvest date, although the probability of success was much greater. The simulated run for 25-percent moisture corn gave a 70-percent probability of success for a 2.7-degree (F) temperature rise and a 75-percent chance of success for the two higher temperatures (table 7). Even by assuming the later harvest date, the top layer could

Table 5--Days required to dry bin average and top layer to 15.5-percent moisture, and accumulated deterioration, assuming September 15 harvest date, 22-percent moisture corn, and 5-hp fan

	Temp	rise 2.	7 degr	rees (F)	Temp.	rise 5.	7 4	egrees (F)	Temp	rise 8.	7 deg	rees (F)
Vear	Av	Average	Top	layer	Ave	erage	Top	layer	Av	erage	Top	layer
1 3 3	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration
	No.	Percent	No.	Percent	No.	Percent	No.	Percent	No.	Percent	No.	Percent
											,	•
1955	6	0.354	19	∞	∞	35	16	9	_ '	2 .	14	0.456
1956	9:	.144	12	-	9	2	11	22	٠ ک	14 7	11 1,1	7 (
1957	: 12	. 257	19	39	11	25	17	38	10	27	7. To	7 1
1958	: 13	. 434	20	.508	11	.423	7 7	.530	0T	.4T4 322	17 17	967
1959	: 11	.409	7 7	7	٧	4	0 T	7	0	1	+	•
1000		37	8	7 7	10	7	16	.434	7	.250	14	\vdash
1061	71.	9,66	200	33	1 2	. 4	18	.334	10	7	15	2
1061		007.	27	76	1 9 1	. О	23	0	13	.590	19	9
1962	07.	617	19	.725	12	.625	17	.731	10	.571	16	.742
1967	F	. 503	23	53	14	9	20	.546	12	.394	18	51
+00+) - -))									
1965	: 22	767.	27	4		3	24	0	15	.397	21	.462
1966	. 15	41	22	∞	13	∞	19	∞	11	3	17	∞
1967		.338	18	.420	6	.297	16	.418	∞	∞	14	42
1968	. 10	29	16	∞	6	9	15	9	∞	9	14	37
1969	: 15	62	21	85	14		19	∞	12	4	17	2
			,	,				0.0		~		7.
1970	: 16	.478	22	.602	14	.453		$^{\circ}$	77	4 6		. 200. 315
1971	: 15	.270	21	.377		. 210		.347		$^{\circ}$		ر د د
1972	: 10	.310	17	.423	6	300	15	.431	ρç	2067.	1 T	524.
1973	: 19	. 539	25	009.	15	.435		900°	77	ν c		020.
1974	: 14	.344	21	.418	12	.329		.417	12	. 7		.472
Average	: 14	.411	20	.510	12	.380	18	.471	10	.351	16	.460
Probability												
of success (≥0.5%)		75		09		85		09		85		70

not be solar dried fast enough in years of bad weather to prevent spoilage. More important, adding 3 degrees (F) increased the accumulated grain deterioration in the top layer 70 percent of the time. Effects of added solar heat on the deterioration rate are shown in figure 3.

Fan size was increased to 10 hp for years that deterioration exceeded 0.5 percent in the first October 15 run, raising the probability of success for all temperature levels to 85 percent.

The time required to dry the top level to 15.5-percent moisture was reduced by 1 to 13 days for the years of failure, assuming the 5-hp system.

For a selected poor-drying year, solar drying was simulated for corn harvested at 22- to 25-percent moisture. As beginning

Table 6--Effect of early maturity on grain deterioration, given unfavorable postharvest drying weather, September 15 harvest date, 5-hp fan

Temperature rise and grain	Corn moi	sture (percent	•
deterioration	25	: : 22	deteri- oration
		Percent	
		rercent	<u>:</u>
2.7 degrees (F)	•		
temperature rise:	·		
Average deterioration	0.586	0.207	-0.379
Top layer deterioration:	1.150	.375	775
;	•		
5.7 degrees (F)	;		
temperature rise:	:		
Average deterioration	.514	.177	337
Top layer deterioration:	1.136	.336	800
0.7.1			
8.7 degrees (F)			
temperature rise:			
Average deterioration :	.473	.159	314
Top layer deterioration:	1.066	.324	742
:	· · · · · · · · · · · · · · · · · · ·		

Table 7--Days required to dry bin average and top layer to 15.5-percent moisture, and accumulated deterioration, assuming October 15 harvest date, 25-percent moisture corn, and 5-hp fan

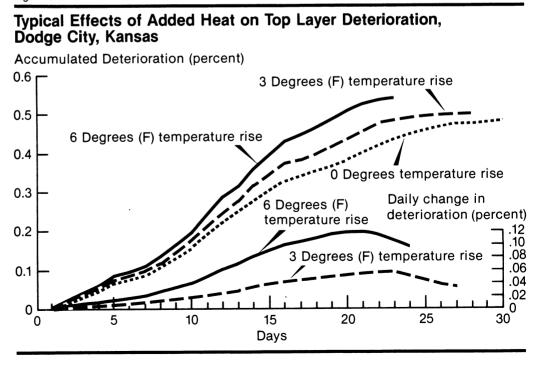
	Temp.	p. rise 2.	7	degrees (F)	Temp.	. rise 5.	_	degrees (F)	Temp.	. rise 8.	_	degrees (F)
Year	. A.	Average	Top	layer	Av	Average	Top	layer		Average	Top	layer
	: Days	Deteri- s oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration	Days	Deteri- oration
	No.	Percent	No.	Percent	No.	Percent	No.	Percent	No.	Percent	No.	Percent
1955	: 12	0.191	19	0.233	11	0.200	18	25	10	0.211	16	_
1956	: 16	.397	24	•	13	ຕຸ	21	.47	12	ິຕ	19	.47
1957	: 33	.441	39	. 504	23	4	31	44	18	\sim	26	43
1958	: 11	.188	20	.239	13	.184	18	.255	6	. 204	16	.269
1959	: 19	.321	28	.368	14	.273	23	_	12	.281	20	/
	••	•	(,	(1	1	1	,	,	
1960	: 24	644.	32	. 484	19	\sim	27	. 500	17	9	23	3
1961	: 13	.181	23	. 282	11	.172	19	.279	10	.183	18	.277
1962	: 17	. 289	25	. 330	14	∞	22	.347	13	∞	19	4
1963	: 19	.812	76	668.	16	3	23	.918	14	3	20	9
1964	: 19	.461	28	.538	16	/	22	.490	13	9	20	9
	••											
1965	: 20	.550	29	. 693	17	.528	25	.662	15	.517	21	099.
1966	: 15	.161	24	. 204		2	22	.217		.147	19	\sim
1967	: 11	.132	19	.173		3	18	.184		.142	16	9
1968	: 16	.263	24	. 336		/	21	.345	13	. 269	19	<⁺
1969	: 29	.443	37	.481		7	31	.485		· 404	28	9
0701	•	000	3.6	C	Ç	-		Ų		-	Č	170
1970	07.	. 323		673	70	٦ ،		1 0		٦,	07	.507
1072		ノし	ر د	. 740	1.7 2.1) 4		· c		$^{\circ}$	67	200.
1973	. 12	7,7	20	. 547 315	11	7		7 ~		γ α	17	262.
1974	: 28	. 748	33	.757	18	.667	27	747.	15	. 599	22	.761
	••											
Average	: 19	.370	27	.427	16	.353	23	.405	14	.347	21	.435
Probability												
of success (≥0.5%)		80		70		80		75		80		75
	• ••)) •))		

moisture content was lowered, deterioration of the top layer was reduced as follows:

Percentage	Tempera	ature rise	(degrees (F))
moisture	2.7	5.7	8.7	7
	Per	rcent deter	cioration	
25	0.693	0.662	0.66	50
24	.485	.480	.47	77
23	.351	.346	.34	4 5
22	.253	. 250	.25	50

Regardless of harvest dates, the single-fill strategy consistently produced overdried corn. To reduce the top layer to 15.5-percent moisture, the bin average moisture frequently reached 11.5 to 12 percent. This practice, of course, would lead to profit losses. A bushel of corn, at 11.5-percent moisture, wet basis, weighs about 53.5 pounds. Assuming corn valued at \$2.50 per bushel (4.5 cents per pound), this strategy could result in a loss of 11.2 cents per bushel due to excessive moisture loss alone.

Figure 3



Transfer Strategy

The strategy of transferring partially solar dried corn to a storage bin may be preferable to the single-fill strategy. Wet and dry corn--corn above and below 15.5-percent moisture--is assumed to be well mixed at the time of transfer with equilibration taking place in about 2 days. Transferring corn to a storage bin accomplishes two things: it sharply reduces the number of days that the top layer(s) of grain remains at the high-moisture content, and it minimizes the number of days the drying bin is used per batch.

September 15 Harvest Date. Whereas deterioration consistently exceeded 0.5 percent while waiting for the top layer of September 15 harvested corn (25-percent moisture) to reach 15.5-percent moisture content, the probability of success was much greater if the corn was held in the drying bin only until the average moisture content reached 15.5 percent. The probability of success, assuming a 5-hp fan, was 60 to 80 percent for these temperature levels (table 4). The number of drying days was reduced as follows:

Ctratagy	Temperature	rise ((degrees (F))
Strategy	2.7	5.7	8.7
	Average	number	of days
Top layer dried to	23	21	19
Bin average dried to 15.5 percent	17	15	13
Savings in time	6	6	6

Even with this time savings, the allowable storage time for shelled corn was exceeded in some years. Thus, it can be concluded that it is not advisable to use low-temperature solar drying when following either of the batch-in-bin drying strategies if the farmer desires to harvest high-moisture corn on September 15 in the west central Great Plains.

For the simulation run assuming a September 15 harvest date and 23-percent moisture corn, the transfer strategy yielded an 85-percent probability of success when solar heat was added (table 5). This compared with a 75-percent probability without additional heat and only a 60-percent probability of success for the single-bin strategy. The addition of 3 degrees (F) of heat increased the probability of successful drying from 75 to 85 percent. The addition of 6 degrees (F) of solar heat failed to

improve the probability of success. The time required for the average moisture content to reach 15.5 percent, assuming a 2.7-degree (F) temperature rise (0 degrees added solar heat), averaged 14 days, 6 days faster than for the single-bin strategy. The addition of 3 degrees (F) solar-supplemented heat reduced the drying time 2 additional days. Both cumulative deterioration and days of drying time were reduced when lower moisture grain was harvested (fig. 4).

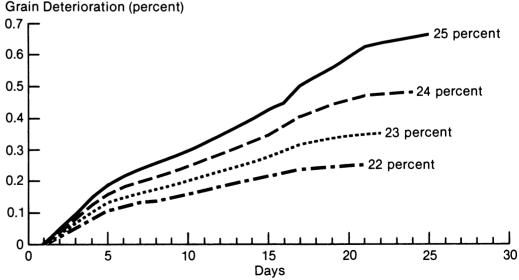
Simulation runs assuming 22-percent moisture corn showed a 100-percent probability of successful drying without adding heat beyond that produced by the 5-hp fan. About 7 fewer days were required to dry 22-percent moisture corn than 25-percent moisture corn.

October 15 Harvest Date. The simulation runs for an October 15 harvest date, assuming 25-percent moisture corn, resulted in an 80-percent probability of success regardless of the temperature rise (table 7).

By increasing the fan size to 10 hp, the probability of successful drying increased to 90 percent when no heat was added. The probability of success increased to 95 percent in both solar heat situations.

Figure 4

Effects of Corn Moisture Content on Cumulative Deterioration of Top Layer in Bin and Drying Time¹



1Simulated results based on October 15 harvest date, 5-hp fan, and 5.7 degrees (F) temperature rise.

The number of days required to dry the average bin content of 15.5-percent moisture was sharply lowered by using the transfer strategy:

G	Temperature	rise (de	egrees (F))
Strategy	2.7	5.7	8.7
	Average	number	of days
Top layer dried to	27	23	21
Bin average dried to 15.5 percent	19	16	14
Savings in time	8	7	7

When following the transfer strategy, the FALDRY model suggests that there is little advantage in delaying harvest until corn is below 25-percent moisture. Likewise, no advantage exists for solar-supplemented heat when harvesting corn in the region on October 15. When weather conditions in the west central Great Plains are conducive to drying shelled corn, it can be dried with natural air. If weather conditions are not conducive to drying, a few degrees of supplemental solar heat will not help. In fact, in most years, a few degrees of supplemental heat increases deterioration in the top layer of the drying bin (fig. 3).

Thus, the simulation results suggest that achieving a high degree of low-temperature solar drying success relies on a corn harvest in the west central Great Plains after September 15 unless the moisture content is below 23 percent. The results also show that a solar-supplemented system would work in a single-bin strategy, but a natural air system will perform just as well given proper airflow. The grain temperature and the number of days required to dry the average moisture content of the corn to 15.5 percent, and the resultant accumulated top layer deterioration, are shown in appendix tables 4 and 5.

Layer-in-bin Drying

A layer-in-bin drying method could be used on farms with two or more drying/storage bins or when a fast harvest is not critical. As the concept suggests, successive layers of grain are placed in a drying bin until it is filled, assuming that the corn continued to dry 0.5 percent per day in the field before harvest. Layer depths are determined by the cubic-feet-per-minute output of the drying fan and the moisture of the grain to be solar dried.

Proper layer depth is determined by checking the bin for the highest point dried on the morning following the placement of the wet grain (2). This is called the drying point. If it is within 6 inches of the top of the layer, the system—fan and depth of layer—is in balance.

Years of exceptionally high top layer deterioration were selected from the previous runs to simulate layer-in-bin drying. One year--1963--typified the improved performance of layer-in-bin drying over batch-in-bin drying (table 8). The data show the importance of placing high-moisture grain in bins at only shallow depths when using low-temperature solar drying.

According to the results of the simulation runs for 1963, a poor drying year, layer-in-bin drying reduced the time required to dry the top layer of shelled corn to 15.5-percent moisture by 2

Table 8--Comparison of shelled corn deterioration, by method of solar drying and temperature rise $\underline{1}/$

D 1	:	Tempera	ture rise	(degrees (F))
Drying strategy	: :	2.7	5.7	8.7
	:			
	:			
Batch-in-bin:	:			
Average deterioration	:	0.478	0.463	0.454
Top layer deterioration	:	.899	.918	.960
. ,	:			
Layer-in-bin (2-day	:			
fill interval):	:			
Average deterioration	:	.211	.188	.169
Top layer deterioration	:	.303	.300	.298
	•			
Layer-in-bin (5-day	:			
fill interval):	:			
•	•	.063	.049	.040
Average deterioration	•			
Top layer deterioration	:	.043	.038	.033
	:			

¹/ Simulated data for October 15, 1963 harvest, a year of exceptionally poor drying weather in the Dodge City region.

to 5 days, depending on the interval between fillings:

Strategy	Temperature	rise (d	egrees (F))
Strategy	2.7	5.7	8.7
		Days	
Batch-in-bin Layer-in-bin	26	23	20
Fill interval: 2-day 5-day	24 21	20 17	18 16

Results of five simulation runs, shown in table 9, indicate two things: that 25-percent moisture corn can be successfully dried every year, even if harvested early in the fall; and that solar-supplemental heat is advantageous, decreasing both drying time and top layer deterioration.

The simulation runs for layer-in-bin drying reflected no increases in top layer deterioration when solar heat was added. However, this method, like the batch-in-bin strategy, resulted in appreciable overdrying.

Thus, while the layer-in-bin strategy appeared to yield better results than the batch-in-bin strategy, neither yielded the results expected for a region with abundant solar radiation. In this region, farmers may benefit most by using no supplemental heat.

ANNUAL COSTS

Annual ownership and operating costs of the grain drying/storage system are estimated to be 66.8 cents per bushel. These costs reflect 100-percent utilization of the storage space for a 6-month period each year.

Fixed Costs

Fixed costs totaled 53.2 cents per bushel and accounted for 80 percent of all costs (table 10). The cost of the solar collector and equipment was calculated at 2.5 cents per bushel for 2-months use. This cost included a 5-hp fan and related ductwork. In reality, this equipment would be necessary just to operate the natural air system. As shown in table 3, the fans cost \$660, or two-thirds of the total investment charged for the solar collector and related equipment. Thus, the use of solar energy as a supplement to natural air added only the cost of the collectors and the transition equipment for connecting the fans to the solar collectors. This added investment of \$1,119 resulted in annual fixed costs totaling 2.5 cents per bushel.

Table 9--Predicted drying results, assuming layer-in-bin strategy, selected harvest dates

	Filling :	Beginr moisture	Beginning sture content	ent	Da	Days to dry by temperature rise	a)		Top	
Harvest date	interval:	ρλ	by layer	••	1	. 200200	2002207	·••	Layer	ç
		T	2	3	(F)	(F)	(F)			
	Days	1 1 1	Percent -	1	1 1 1 1	<u>Days</u>		 	- Percent -	1 1
October 15, 1963	2	25	22.5	20	21	1.7	16	0.043	0.037	0.033
October 15, 1963		25	24	23	24	20	18	.303	300	.298
October 1, 1963	5	25	24	23	13	12	12	.104	.100	660.
October 1, 1965		25	24	23	20	18	16	.238	.189	.167
October 1, 1974		25	24	23	22	20	18	.218	.202	.193
	••									

Table 10--Fixed costs of owning an 8,000-bushel grain-drying and storage system, using solar energy to supplement natural air drying, 1980

Item	Cost
	: Cents per bushel
Bins and accessories:	: :
Depreciation	: 8.7
Interest on investment	: 12.2
Taxes	: 3.8
Insurance	: 1.6
Subtotal	: : 26.3
Handling equipment:	: :
Depreciation	: 6.5
Interest on investment	: 5.3
Taxes	: 1.7
Insurance	.7
Subtotal	14.2
Aeration equipment:	: :
Depreciation	: .9
Interest on investment	: .7
Taxes	: .2
Insurance	<u>1</u> /
Subtotal	1.8
Solar collector and equipment (2 months):	: :
Depreciation	: 1.3
Interest on investment	: .8
Taxes	: .3
Insurance	: .1
Subtotal	: : 2.5
Quality control:	: :
Depreciation	.8
Interest on investment	: .5
Taxes	: NA
Insurance	: NA
Subtotal	: 1.3
Total	: : 46.1

NA = Not applicable.

^{1/} Less than 0.05 cent.

Variable Costs

Variable costs totaled 13.6 cents per bushel, or 20 percent of all costs (table 11). Costs related to the solar collector included the fan operation cost, labor, and repairs. However, as explained previously, the fan would have been operated regardless of solar collector use. Therefore, the only added variable costs charged to the solar collectors were the repair and labor costs, totaling 2.4 cents per bushel.

Total Costs

In these cost analyses, the bin, handling, and quality control costs were assumed to be incurred by the storage function, even if the corn had not been dried. The fixed and variable costs directly associated with the solar collector totaled only 4.9 cents per bushel. This cost equaled about one-half of the discount (10 cents per bushel) had corn gone out of condition and been graded No. 3 instead of No. 2.

Table 11--Variable costs of operating an 8,000-bushel graindrying and storage system, using solar energy to supplement natural air drying, 1980

Item	:	Cost
	:	
	:	
	•	Cents per bushel
	•	
Insurance	•	1.1
Instrance	•	1.1
Tours to section 1	•	E
Insect control	•	.5
	:	
Handling	:	.8
	:	
Aeration	:	.6
	:	
Solar drying (electricity, 3.0;	:	
labor, 0.4; and repair, 2.0)	:	5.4
,,,,	•	
Interest on operating capital	•	. 2
interest on operating capital	•	• •
Wedget loss	•	5.0
Weight loss	•	J. U
m . 1	:	12.6
Total	:	13.6
	:	

Fixed and variable costs directly associated with solar drying and natural air drying were just about equal to the 10-cent cash discount for No. 3 corn. These costs include:

Item	Cents per bushel
Fixed costs: Aeration Solar-related	1.8 2.5
Subtotal	4.3
Variable costs: Aeration Solar-related Subtotal	0.6 5.4
Total costs	10.3

CONCLUSIONS

Results of the FALDRY simulation model show that supplemental-solar drying is neither necessary nor successful every year in the west central Great Plains. A comparison of drying costs and cash premiums for high-quality corn suggests that even if solar-supplemented heat could be used successfully every year, farmers would not be economically rewarded for their efforts. Costs of solar-supplemented drying exceeded the prorated economic losses due to corn deterioration. This finding suggests the possibility that farmers may market lower quality corn if fuel shortages cause them to use low-temperature solar or natural air drying methods and if they are not economically rewarded for producing No. 2 grade corn.

Since results of the study showed that corn deteriorated even with solar-supplemented heat in poor drying years, it may also be concluded that high-speed, high-temperature drying is necessary to avoid field losses and ensure the marketing of high-quality corn.

Previous studies throughout the Corn Belt have shown that solar collectors are not a reliable source of energy for drying grain every year. The probability of successful solar drying is higher in the Dodge City area than in the Corn Belt. Therefore, the results of this economic analysis are assumed to be reasonably accurate for corn-producing areas. Also, the minimal economies associated with the solar drying function suggest that the economics of using a solar-supplemented system would be about the same for larger systems.

Further research is needed on the use of solar collectors to supplement natural air drying of batch-in-bin systems with more shallow depths of grain and larger diameter bins.

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Appendix table 1--Days required to dry top layer of corn to 15.5-percent moisture, average grain temperature, and accumulated deterioration of the top layer $\underline{1}/$

Year			__\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	•	1905 0011	(T) 600 190n	·	7.10.01.10.001.10	(-)
	Days required	Grain 1 temperature	Deteri- oration	Days required	Grain temperature	Deteri- oration	Days required	Grain temperature	Deteri- oration
	No.	Degrees F	Percent	No.	Degrees F	Percent	No.	Degrees F	Percent
955	25	99	1.681	22	57	1.502	19	78	1.281
926	14	99	.379	12	9/	.393	12	78	.510
9	: 21	72	.777	19	74	.753	18	74	.736
σ	: 22	70	.940	20	70	.933	19	70	686.
: 6561	: 25	54	1.010	21	09	.981	18	57	766.
. 096	. 22	19	1,123	20	68	1.065	18	09	1,006
1961	22	1 89	•	21	29	•	19	99	.623
	30	61	2.654	<u></u> 56	71	2.174	22	89	1.597
963	21	72	•	19	73	•	18	9/	1.392
. 496	: 25	57	.947	23	58	.988	21	09	1.049
965	30	70	1.150	26	70	1.136	24	89	1.066
996	25	63	.980	22	29	•	20	62	646.
1967	: 20	74	.877	19	77	.826	17	74	962.
896	: 18	63	.756	17	75	. 785	16	77	.735
: 696	: 24	7 9	2.183	21	09	1.944	20	80	1.845
026	25	43	1.286	22	73	1.147	20	74	1.202
971	24	59	•	21	65	•	19	63	.735
972	: 20	99	.839	18	69	.842	16	63	.858
1973	: 27	52	1.416	25	77	1.272	22	70	1.236
974 ;	: 23	55	.907	21	74	.817	19	73	.817

1/ Assumes September 15 harvest date, 25-percent-moisture corn, and 5-hp fan.

Appendix table 2--Days required to dry top layer of corn to 15.5-percent moisture, average grain temperature, and accumulated deterioration of the top layer $\underline{1}/$

	Temp.	rise 2.7 degr	ees (F)	Temp.	rise 5.7 degrees	ees (F)	Temp.	rise 8.7 deg	degrees (F)
Year	Days	Grain	Deteri- oration	Days	Grain temperature	Deteri- oration	Days required	Grain temperature	Deteri- oration
	No.	Degrees F	Percent	No.	Degrees F	Percent	No.	Degrees F	Percent
955	. 19	71	0.428	16	65	0.460	14	75	0.456
1956	: 12	72	.219	11	73	.227	11	9/	.237
957	: 19	69	.394	17	71	.383	16	74	.372
958	: 20	99	.508	18	57	.530	16	58	.530
959	: 18	52	.497	16	53	967.	14	99	964.
	••								
096	: 18	99	.454	16	09	.434	14	72	.419
961	: 20	09	.328	18	56	.334	15	7.5	.329
962	: 27	89	.941	23	99	.823	19	65	.765
963	: 19	70	.725	17	70	.731	16	89	.742
1964	: 23	61	.538	20	26	.546	18	63	.516
	••								
965	: 27	26	.548	23	65	. 509	21	99	.462
996	: 22	65	.486	19	9	.487	17	61	.481
196	: 18	72	.420	16	71	.418	14	61	.420
896	: 16	71	.383	15	71	.395	14	75	.378
1969	: 21	57	.852	19	78	.786	17	75	.353
	••								
970	: 22	71	.602	20	71	.579	18	70	.557
971	: 21	62	.377	19	09	.347	17	78	.315
972	: 17	63	.423	15	57	.431	14	69	.429
973	: 25	74	009.	21	59	.559	19	89	.526
974	: 21	72	.418	18	62	.417	17	99	.425
	• (

1/ Assumes September 15 harvest date, 23-percent-moisture corn, and 5-hp fan.

Appendix table 3--Days required to dry top layer of corn to 15.5-percent moisture, average grain temperature, and accumulated deterioration of the top layer $\underline{1}/$

Year Days required required No.	Grain ed temperature					••		
955 N 956 959 960 961 965 965 966 965 966 966 966 966 966 966 966 966 966 966		Deteri- oration	Days	Grain temperature	Deteri- oration	Days required	Grain temperature	Deteri- oration
955 : 956 : 960 : 964 : 965 : 966 :	Degrees F	Percent	No.	Degrees F	Percent	No.	Degrees F	Percent
956 : 957 : 958 : 959 : 959 : 959 : 960 : 962 : 964 : 966 :	40	0.233	18	50	0.252	16	53	0.274
957 : 959 : 959 : 959 : 960 : 964 : 965 : 966 : 966 : 966 : 967 : 968 : 969 :	45	.451	21	45	47	19	51	7.7
958 : 959 : 960 : 962 : 964 : 965 : 966 : 966 : 966 : 966 : 967 : 968 : 969 : 969 : 969	97	. 504	31	67	.442	26	48	.439
959 : 960 : 961 : 962 : 964 : 965 : 966 : 966 : 968 : 969 :	51	. 239	18	50	.255	16	49	26
960 : 961 : 962 : 964 : 965 : 966 : 967 : 968 : 969 : 969 : 969 : 969	43	.368	23	33	.375	20	65	3,7
961 : 962 : 964 : 964 : 966 : 966 : 967 : 968 : 969 : 969	50	.484	27	38	.500	23	67	. 535
962 : 963 : 964 : 965 : 966 : 967 : 968 : 969 : 969	34	.282	10	48	.279	18	67	.277
963 : 964 : 965 : 966 : 967 : 968 : 969 : 969	43	.330	22	77	.347	19	51	.343
964 : 965 : 966 : 967 : 969 : 969 : 969	26	668.	23	55	.918	20	56	096.
965 : 967 : 968 : 969 :	54	.538	22	54	.490	20	63	.460
. 996 . 968 . 969	48	.693	25	54	.662	21	56	099
	55	. 204	22	45	. 217	19	38	. 227
: 696 : 696	43	.173	18	52	.184	16	51	.196
: 696	41	.336	21	56	.345	19	09	.345
•	77	.481	31	36	.485	28	57	794.
: 026	46	.359	29	77	.363	26	53	.367
9	26	. 543	26	47	.575	23	41	.612
972 :	97	.347	27	47	.297	24	53	.295
73 :	42	.315	18	57	.337	17	55	.362
: 516	77	.757	27	51	.747	22	63	.761
•								

1/4 Assumes October 15 harvest date, 25-percent-moisture corn, and 5-hp fan.

Appendix table 4--Days required to dry average moisture content of corn to 15.5 percent, average grain temperature, and accumulated deterioration of top layer $\underline{1}/$

Year Days Grain Deterining oration Deterining required Grain 1955 No. Degrees F Percent No. Degrees F 1956 8 61 .154 7 65 1956 8 61 .154 7 65 1956 15 65 .307 13 65 1957 15 65 .307 13 65 1958 16 62 .482 14 66 1958 16 62 .434 14 66 1960 16 62 .434 14 66 1961 16 50 .278 15 55 1962 23 64 .909 19 65 1963 15 51 .531 17 57 1964 19 65 .461 16 65 1965 14 60 .553 10 64 <th>Det ora Per</th> <th>Days</th> <th></th> <th></th>	Det ora Per	Days		
No. Degrees F Percent No. Degree Section Section	s F Percen	required	Grain temperature	Deteri- oration
20 70 0.625 15 8 61 .154 7 15 65 .307 13 16 48 .482 14 18 51 .470 13 18 51 .470 13 16 62 .434 14 16 50 .278 15 15 59 .657 13 19 51 .531 17 14 53 .351 17 14 53 .351 12 12 62 .461 16 14 53 .351 12 12 62 .461 16 13 .300 11 14 53 .351 16 18 61 .805 16 18 61 .392 11 14 61 .392 11 24 61 .392 11 25 13 19	0	No.	Degrees F	Percent
15 65 .307 13 16 48 .482 14 16 62 .470 13 16 62 .434 14 16 50 .278 15 16 50 .278 15 15 59 .657 13 19 51 .531 17 19 51 .531 17 14 53 .351 12 12 66 .461 16 12 66 .805 16 13 .90 11 12 14 53 .351 12 12 66 .805 16 13 .90 11 14 53 .351 16 18 61 .573 16 14 61 .395 15 14 61 .395 11 21 .20 .20 .20 14 61 .295 15 <tr< td=""><td>•</td><td>13</td><td>73</td><td>0.464</td></tr<>	•	13	73	0.464
15 65 .307 13 16 48 .482 14 18 51 .470 13 16 62 .434 14 16 50 .278 15 23 64 .909 19 15 59 .657 13 19 51 .531 17 14 53 .351 17 12 62 .461 16 12 62 .461 16 12 62 .300 11 12 66 .805 16 13 .53 .295 15 14 61 .573 16 18 59 .295 15 14 61 .392 11 21 65 .295 19		7	29	.163
16 48 .482 14 18 51 .470 13 16 62 .434 14 16 50 .278 15 15 50 .278 15 15 59 .657 13 15 59 .657 13 19 51 .531 17 14 53 .351 12 12 62 .461 16 12 62 .300 11 17 66 .805 16 18 61 .573 16 18 59 .295 15 14 61 .392 11 21 66 .295 15 14 61 .392 11 21 62 .295 19	•	11	99	.260
18 51 .470 13 16 62 .434 14 16 50 .278 15 23 64 .909 19 15 59 .657 13 19 51 .531 17 19 51 .531 17 14 53 .461 16 12 62 .461 16 12 62 .351 12 14 53 .351 12 17 66 .805 16 18 61 .573 16 18 59 .295 15 14 61 .392 11 21 66 .295 19 21 67 .295 19	•	12	58	.448
16 62 .434 14 16 50 .278 15 23 64 .909 19 15 59 .657 13 19 51 .531 17 24 60 .558 20 18 62 .461 16 14 53 .351 12 12 66 .805 16 13 66 .805 16 18 59 .295 15 14 61 .554 19	•	11	65	.418
16 62 .434 14 16 50 .278 15 23 64 .909 19 15 59 .657 13 19 51 .531 17 24 60 .558 20 18 62 .461 16 14 53 .351 12 12 66 .805 16 13 66 .805 16 18 61 .573 16 18 59 .295 15 14 61 .392 11 54 61 .554 19				
16 50 .278 15 23 64 .909 19 15 59 .657 13 19 .657 13 24 60 .558 20 18 62 .461 16 14 53 .351 12 12 62 .360 11 12 66 .805 16 18 59 .295 15 14 61 .392 11 21 61 .392 11 21 54 61 .554 19	•	13	99	.373
: 23 64 .909 19 : 15 59 .657 13 : 19 51 .531 17 : 24 60 .558 20 : 18 62 .461 16 : 14 53 .351 12 : 12 62 .300 11 : 17 66 .805 16 : 18 61 .573 16 : 18 59 .295 15 : 14 61 .392 11 : 14 61 .392 11 : 21 54 554 19	•	13	09	.268
: 15 59 .657 13 : 19 51 .531 17 : 24 60 .558 20 : 18 62 .461 16 : 14 53 .351 12 : 12 62 .300 11 : 17 66 .805 16 : 18 61 .573 16 : 18 59 .295 15 : 14 61 .392 11 : 27 54 19	674.	15	63	.615
: 19 51 .531 17 : 24 60 .558 20 : 18 62 .461 16 : 14 53 .351 12 : 12 62 .300 11 : 17 66 .805 16 : 18 61 .573 16 : 18 59 .295 15 : 14 61 .392 11 : 21 54 554 19	•	12	29	.617
24 60 .558 20 18 62 .461 16 14 53 .351 12 12 62 .300 11 17 66 .805 16 18 61 .573 16 18 59 .295 15 14 61 .392 11 21 54 55 19	•	15	70	.475
: 24 60 .558 20 : 18 62 .461 16 : 14 53 .351 12 : 12 62 .300 11 : 17 66 .805 16 : 18 61 .573 16 : 18 59 .295 15 : 14 61 .392 11 : 21 54 554 19				
: 18 62 .461 16 : 14 53 .351 12 : 12 .300 11 : 17 66 .805 16 : 18 61 .573 16 : 18 59 .295 15 : 14 61 .392 11 : 27 54 554 19	7474	18	63	.438
14 53 .351 12 12 62 .300 11 17 66 .805 16 18 61 .573 16 18 59 .295 15 14 61 .392 11 21 54 554 19	•	14	29	.413
: 12 62 .300 11 : 17 66 .805 16 : 18 61 .573 16 : 18 59 .295 15 : 14 61 .392 11 : 21 54 554 19	•	10	64	306
: 17 66 .805 16 : 18 61 .573 16 : 18 59 .295 15 : 14 61 .392 11 : 21 54 554 19	•	10	65	.287
: 18 61 .573 16 6 : 18 59 .295 15 7 : 14 61 .392 11 6 : .7 .5 .19 6	•	14	73	.672
: 18 59 .295 15 7 : 14 61 .392 11 6 : 17 54 19 6	.52	14	62	.512
: 14 61 .392 11 6 : 21 54 54 19 6	. 22	13	70	.184
9 1 25 27 10 6	.35	10	70	.341
0 1	3 .519	16	62	.450
; 16 55 ,386 15 6	.38	13	99	.374

1/ Assumes September 15 harvest date, 25-percent-moisture corn, and 5-hp fan.

Appendix table 5--Days required to dry average moisture content of corn to 15.5 percent, average grain temperature, and accumulated deterioration of top layer 1/

	Temp.	rise 2.7 de	grees (F)	Temp.	rise 5.7 degrees	ees (F)	Temp.	rise 8.7 degrees	ees (F)
Year	 Days required	Grain d temperature	Deteri- oration	 Days required	Grain temperature	teri- ation	 Days required	Days Grain required temperature	Deteri- oration
	No.	Degrees F	Percent	No.	Degrees F	Percent	No.	1	Percent
6	6	09	0.354	œ	73	0.351	7	7.2	0 321
9	9:	65	.144	9	89	•	· 1/	5 y	142
1957	: 12	62	.257	11	62	.258	0 0	67	255
9	: 13	54	.434	11	61	.423	10	74	414
9	: 11	99	.409	6	69	.346	, &	71	.322
	••								
1960	: 12	62	.370	10	65	.341	7	71	.250
1961	: 14	26	.266	11	53	.241	10	26	249
1962	: 20	63	692.	16	61	769.	13	29	590
1963	: 13	63	.617	12	99	.625	10	17	571
1964	: 18	55	.503	14	56	.398	12	63	.394
	••								
1965	: 22	57	.497	18	61	.433	1.5	7 9	397
1966	: 15	62	.412	13	61	.382	11	89	.335
1967	: 11	69	.338	6	63	.297	· ∞	67	. 288
1968	: 10	61	.291	6	70	.298	- ∞	78	. 261
1969	: 15	69	.626	14	71	.618	$1\overline{2}$	72	. 548
	••						l !	1) •
1970	: 16	63	.478	14	09	.453	12	54	.443
1971	: 15	72	.270	13	89	.210	12	69	. 233
1972	: 10	99	.310	6	63	300	, ∞	29	962.
1973	: 19	61	.539	1.5	58	.435	12	65	367
1974	: 14	54	.344	12	65	.329	12	89	.321
	••								

 $\frac{1}{2}$ Assumes September 15 harvest date, 23-percent-moisture corn, and 5-hp fan.

Appendix table 6--Days required to dry average moisture content of corn to 15.5 percent, average grain temperature, and accumulated, deterioration of top layer $\overline{1/2}$

	Temp.	rise 2.7 degr	ees (F)	Temp.	rise 5.7 degrees	ees (F)	Temp.	rise 8.7 degree	rees (F)
Year	Days	Grain d temperature	Deteri- oration	Days	Grain temperature	Deteri- oration	Days required	Grain temperature	Deteri- oration
	No.	Degrees F	Percent	No.	Degrees F	Percent	No.	Degrees F	Percent
5		24	0.191	11	53	0.200	10	51	0.211
1956		51	.397	13	55	.334	12	54	.345
95		40	.441	23	94	.408	18	62	.383
95		67	.188	13	51	.184	6	53	. 204
1959	: 19	53	.321	14	51	.273	12	97	.281
1960	24	45	644.	19	50	.436	17	67	.461
1961	13	57	.181	11	97	.172	10	54	.183
$\frac{1962}{1962}$: 17	51	. 289	14	52	. 282	13	63	.284
1963	: 19	97	.812	16	58	.832	14	52	.836
1964	: 19	63	.461	16	63	.379	13	63	. 293
96	20	55	.550	17	54	.528	15	09	.517
96	. 15	47	.161	13	58	.150	12	58	.147
1967	: 11	87	.132	10	50	.139	6	61	.142
96	: 16	59	.263	15	57	.272	13	51	. 269
96	: 29	50	.443	25	53	.425	22	54	. 404
1		L	Ċ	ć	ī	216	0	7.7	21.3
1970	97	4.0	. 525	67	TC ,	010.	O L	† °	
1971	: 23	34	.512	19	94	.535	T2	43	.533
1972	24	45	.273	21	53	.258	17	38	.253
1973	: 12	54	. 263	11	26	.275	10	59	. 286
1974	: 28	43	. 748	18	54	.667	15	63	. 599

Assumes October 15 harvest date, 25-percent-moisture corn, and 5-hp fan.

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